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Impact of particle size and catalyst dispersion on gasification rates measured in a thermogravimetric analysis unit: Case study of carbon black catalyzed by potassium or calcium

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- 13 Abstract

14 Gasification is often studied in the laboratory using a thermogravimetric analysis (TGA) unit with

15 less than 1 g of sample in order to obtain intrinsic rates. Many studies, however, neglect to consider 16 the impact of particle size, of both the gasification feed and the catalyst, and catalyst dispersion on 17 the measured rates. The impact of these factors was demonstrated using catalytic gasification of 18 carbon black, an ash-free feed, as a case study, with K₂CO₃ or CaCO₃ as catalysts at 850 °C in a 19 CO₂ atmosphere. Hand-mixing and ball-milling were used to alter the initial parameters. Ball-20 milling reduced both the particle size of both species and increased the catalyst dispersion, 21 resulting in higher interfacial areas and gasification rates than hand-mixing. The changes in

- 22 gasification kinetics were estimated by modeling the rates using the random pore and extended

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random pore models (RPM and eRPM, respectively). The impact of the interfacial contact area
between carbon and catalysts (varied by particle size and mixing method) was dependent on the
activity of the catalyst with the more active (potassium) catalyst being less affected. CaCO₃ was
found to sinter at 850 °C, reducing available catalytic surface area and blocking CO₂ access to the
carbon feed. It is recommended to consider these factors in future studies and to always report the
particle sizes used.
Highlights

- Gasification of carbon black mixed with K or Ca catalysts by different methods
- Dispersion more important as activity of catalyst decreases
- Catalyst size had more impact than carbon black size, confirmed by modeling
- Knowledge of phase behavior softening and sintering temperatures required
- eRPM describes the gasification behavior of catalyzed carbon black
- 36
- 37 Keywords
- 38 gasification; potassium; calcium; ball-milling; catalyst; random pore model

- 40 1. Introduction
- 41 Gasification is used to convert carbon-based feeds to fuels/chemical precursors, such as H₂, CO,
- 42 and CH₄, and can be enhanced by the presence of catalysts, such as calcium and potassium, added

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43 to the feeds prior to gasification or intrinsically present in the feeds [1]. The limiting step in 44 gasification can either be external mass transfer of the gasification agent through the boundary 45 layer, internal mass transfer of the gasification agent through pores to reach active sites, or the surface gasification carbon-oxygen reaction [2]. In the absence of mass transfer limitations, the 46 gasification rate is proportional to the surface area [3], or in the case of low catalytic loadings, the 47 48 number of catalytic sites [4]. At the lab scale, gasification kinetics are commonly determined using 49 a thermogravimetric analysis (TGA) instrument with sample sizes of less than 1 g (often less than 50 10 mg) to avoid mass transfer limitations [5-8]. Decreasing the particle size of the feed increases 51 the surface area and the number of available active sites for gasification [9]. The rate of catalytic gasification is also increased by increased catalyst-carbon interfacial area [10,11], which is 52 53 improved by increasing the dispersion of the catalyst.

54

55 Both wet impregnation [12–19] and physical mixing [13,16,20] have been used to combine the 56 feed with the catalytic species. Wet impregnation results in better dispersion of water-soluble 57 catalytic species, and Kapteijn et al. [21] noted the importance of catalyst dispersion in their survey 58 of alkaline-earth-catalyzed gasification literature. Wet impregnation, however, is ineffective for 59 hydrophobic feeds because the catalytic species are deposited on the surface and not in the pores 60 [22]. Wet impregnation is also ineffective for sparingly soluble catalyst precursors, such as 61 Ca(OH)₂ and CaCO₃. Ash-free coal is an example of a hydrophobic material for which preparation 62 methods other than wet impregnation must be used [23]. Surface groups on hydrophobic materials

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63 can enhance gasification for hydrophobic or non-porous feeds. For example, potassium addition 64 was more effective for increasing the gasification rate of raw petcoke than petcoke char because 65 pyrolysis at 975 °C removed the surface groups (including aliphatic, phenolic, aromatic, and hydroxyl groups) which served as anchoring sites for potassium in the raw coke [24]. Physical 66 mixing is an alternative to wet impregnation for hydrophobic feeds and/or insoluble catalyst 67 precursors, and includes hand and mechanical mixing, such as by crushing [25], or by grinding in 68 69 a rotary tumbler [26] or a planetary ball-mill [27]. The effects of physical mixing techniques on feed properties are rarely discussed in the literature. Hand-mixing, while simpler and less 70 expensive, is less reproducible than mechanical mixing with fixed parameters (e.g., rotation speed, 71 time). One study with raw coal (which is not hydrophobic), claimed that wet impregnation was 72 73 better than physical mixing for the addition of calcium catalysts Ca(OH)₂ and CaCO₃ [28]. This 74 result is surprising given the low solubility of the calcium compounds but the method and details 75 of the physical mixing were not specified, nor were particle sizes or catalyst dispersion. Despite 76 the importance of feed properties on gasification rates, most studies still neglect to consider the 77 effectiveness of the mixing method for reducing particle size and/or increasing catalyst-carbon 78 interfacial area.

79

Herein, we demonstrate the impact of two physical mixing methods, hand-mixing and ball-milling,
to ascertain the effect of feed particle size, catalyst particle size, and catalyst dispersion on catalytic
gasification of carbon black, a model ash-free carbon source, with potassium and calcium. Because

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calcium is less active than potassium due to its lower mobility [16,29–34], the impact of the mixing method was expected to be different for these two catalytic species. Samples were prepared by hand-mixing and/or low-energy ball-milling and characterized using scanning electron microscopy. The samples were gasified in a TGA in a CO₂ atmosphere primarily at 850 °C. The gasification kinetics were modeled using the random pore and extended random pore models.

88

89 2. Materials & Methods

90 2.1 Sample preparation and characterization

91 Carbon black (CB, Monarch 120 from Cabot Corp, Boston, MA) was used as the carbon source. 92 CaCO₃ and K₂CO₃ (>99% purity, Sigma-Aldrich, St. Louis, MI) were the calcium and potassium 93 sources, respectively. The atomic ratio between each metallic element (Ca or K) and carbon was 94 0.1 for consistency with previous publications [35,36]. The high catalyst loading ensured that the 95 number of available catalytic sites was not a limiting factor in the gasification rates. "Hand-mixed" 96 samples were combined by stirring by hand for 5 min, while "ball-milled" samples were combined 97 for 24 h in a low-energy rotary tumbler (model 33B, Lortone, Mukilteo, WA) with zirconia beads 98 5 mm in diameter unless otherwise noted. In some cases, a combination of ball-milling and hand-99 mixing was used. For these experiments, the CB, the catalyst, or both were ball-milled 100 independently for 24 h in the rotary tumbler, and then the CB and catalyst were combined by 101 stirring by hand for 5 min.

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103 CO₂ adsorption analyses were performed to determine the specific surface area of the CB samples.

104 The samples were degassed at 120 °C under vacuum for 6 h. CO₂ adsorption analyses were

105 performed using a Micromeritics Tristar II Plus unit (Norcross, GA) at 273 K, and the microporous

106 surface area was calculated using the 2D-NLDFT model.

107

108 2.2 Gasification

109 Gasification tests were performed using thermogravimetric analysis (TGA) in an SDT Q600 110 instrument (TA Instruments, New Castle, DE). For each experiment, 3.5 mg of sample was heated 111 under N₂ flow (200 mL/min) at 20 °C/min to 850 °C, then CO₂ (200 mL/min) was introduced as 112 the gasification agent. Two experiments were performed at 1000 °C for comparison. A 5 mL/min 113 flow of N₂ was maintained during gasification to limit the backflow of CO₂ to the TGA balance. 114 Weight vs. time data was smoothed to 1000 points by means of the locally estimated scatterplot 115 smoothing (LOESS) technique using SigmaPlot v14.0. In the LOESS technique, a polynomial of 116 a specified order (a third-order polynomial was used herein) is fit to a specified fraction of nearby 117 data (5% was used herein) for each data point using a weighted least squares fit, and then used to 118 determine a weighted average for each data point. Conversion, X, was calculated using Eq. 1:

$$X_t = \frac{m_0 - m_t}{m_0 - m_f}$$
(1)

where *m* denotes mass, and the subscripts 0, t, and f denote the initial value, the value at time t, and the final value, respectively. The rates of reaction were calculated using numerical integration (Eq. 2):

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$$rate(t_1) = \frac{dX}{dt}(t_1) = \frac{X_{t_2} - X_{t_1}}{t_2 - t_1}$$
(2)

where the subscripts *1* and *2* denote two consecutive time points, with 50 data points collected per
minute. The gasification experiments were continued until the mass remained constant for 5 min.
The length of experiments varied between 30 min to 100% conversion (samples V to VII, Table
and 16 h to 53% conversion (sample VIII, Table 1). The TGA was only able to record 16 h of
data, after which experiments had to be terminated.

127

128 2.3 Scanning electron microscopy

129 Scanning electron microscopy (SEM) was used to determine particle size in the prepared mixtures, 130 and to qualitatively assess the extent of mixing. SEM images were obtained (ex situ, ambient 131 temperature and pressure) using a Phenom ProX electron microscope (Thermo-Fisher Scientific, 132 Waltham, MA) with energy-dispersive X-ray (EDX) spectroscopy capabilities. The particle size 133 was estimated from the SEM images using the software ImageJ. A representative SEM image with 134 approximately 100 particles was chosen for each sample, and then ImageJ was used to determine 135 the length (i.e. longest dimension) of each particle, from which a mean particle size was estimated. 136 The errors in the particle sizes are reported as a 95% confidence interval.

137

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139 2.4 Kinetic Modeling

140 The results were modeled using the random pore model (RPM, Eq. 3) [37] and the extended 141 random pore model (eRPM, Eq. 4) [38]:

142
$$\frac{dX}{dt} = k_j (1 - X) \sqrt{1 - \psi \ln(1 - X)}$$
(3)

143

$$\frac{dX}{dt} = k_j (1-X)\sqrt{1-\psi \ln(1-X)} \left(1+c (1-X)^p\right)$$
(4)

145 where k_j is a rate constant and ψ is a structural factor that represents the change in surface area 146 from the initial to the maximum value during gasification. The maximum specific surface area 147 corresponds to the maximum rate of gasification [37]. The eRPM includes two additional semi-148 empirical parameters, *c* and *p*, to represent the shift in the maximum position when catalysts are 149 present during gasification.

150

Kinetic modeling and model discrimination were performed using Athena Visual Studio v14.2 software. In the kinetic modeling, the rate (dX/dt) versus conversion (*X*) data (1000 observations for each sample) was fit to the models by minimization of the residual sum of squares (*RSS*) using the nonlinear least-squares method, determining the values of k_j , ψ , *c*, and *p*. The model discrimination used the Akaike information criterion (*AIC*) [39], defined in Eq. 5:

$$AIC = m \frac{2}{n} + ln\left(\frac{1}{n} RSS\right)$$
(5)

where *m* is the number of estimated parameters, and *n* is the number of observations. For each sample, the model with the lowest *AIC* value (AIC_{min}) was considered the preferred model, which

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usually coincides with higher R^2 values. For further comparison, the relative likelihood L_k (Eq. 6)

and the Akaike probability share π_{AIC} (Eq. 7) were also determined. The relative likelihood L_k compares the *AIC* of a model *k* (*AIC_k*) with the lowest *AIC* among all models (*AIC_{min}*), assuming values between 0 and 1, while the probability share π_{AIC} compares the likelihood of a model *k* with the likelihoods of all the other models.

$$\pi_{AIC} = \frac{L_k}{\sum_{i=1}^k L_k} \tag{6}$$

$$L_k = \exp\left(\frac{AIC_{min} - AIC_k}{2}\right) \tag{7}$$

163

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165 3. Results & Discussion

166 *3.1 Morphologies of raw materials*

167 Micrographs of the CB, K₂CO₃, and CaCO₃, both as received and after ball-milling, are shown in 168 Fig. 1, with the corresponding particle sizes in Table 1. The CB particles as received were 5-50 169 µm sized clusters containing particles <100 nm in size. The catalyst precursors, K₂CO₃ and 170 CaCO₃, are both crystalline ionic compounds but with different morphologies. Since the 171 carbonates are hydrophilic [40], despite being sparingly soluble in water, the particles 172 agglomerated. As received, the K_2CO_3 crystals existed in agglomerates larger than 200 μ m in 173 diameter and so were crushed using a mortar and pestle before use. After crushing, the largest 174 K₂CO₃ agglomerates were 60 µm in size. The particle size of K₂CO₃ (Table 1) was reported as the 175 size of the crystals, not the agglomerates, because the K₂CO₃ agglomerates dispersed into crystals 176 1.5 µm in length during the heating of the gasification experiments. CaCO₃ was present in cubic 177 crystals approximately 7.1 µm in size (Fig. 1c) and at least five times smaller than the K₂CO₃ 178 agglomerates.

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Fig. 1. SEM images of (a) as-received CB, (b) crushed (in mortar and pestle) K₂CO₃, (c) asreceived CaCO₃, (d) ball-milled CB, (e) ball-milled K₂CO₃, and (f) ball-milled CaCO₃. Scale bar in (b) applies to all images.

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Table 1. Particle sizes of pre-gasification mixtures obtained from SEM images (uncertainty represents 95% confidence interval), CO₂ gasification rates at 850 °C after reaching 50% conversion and the times required to reach 50% conversion. Ball-milled components are underlined; mixtures with components ball-milled together are denoted with an asterisk (*).

	Particle size (µm)		Rate at 50%	Time to 50%	
Sample	СВ	Carbonate	conversion (min ⁻¹)	Conversion (h)	
CB (I)	10.6 ± 2.3		0.0016	7.7	
<u>CB</u> (II)	3.1 ± 0.8		0.0022	4.8	
CaCO ₃		7.1 ± 0.8			
K ₂ CO ₃ crystals		1.5 ± 0.2			
CB-K ₂ CO ₃ (III)	7.9 ± 1.7	1.3 ± 0.2	0.0416	0.30	
<u>CB</u> -K ₂ CO ₃ (IV)	2.3 ± 0.4	1.3 ± 0.3	0.0745	0.09	
$CB-\underline{K_2CO_3}(V)$	9.2 ± 2.0	0.7 ± 0.2	0.2796	0.029	
$\underline{\text{CB}}$ - $\underline{\text{K}}_2\underline{\text{CO}}_3$ (VI)	2.4 ± 0.6	0.9 ± 0.1	0.2805	0.030	
<u>CB-K₂CO₃*</u> (VII)	2.1 ± 0.5	0.5 ± 0.2	0.2751	0.032	
CB-CaCO ₃ (VIII)	12.9 ± 3.7	8.0 ± 1.0	0.0006	15.0	
<u>CB</u> -CaCO ₃ (IX)	3.7 ± 1.2	7.6 ± 0.9	0.0005	7.9	
$CB-\underline{CaCO_3}(X)$	11.8 ± 3.0	1.9 ± 0.6	0.0015	3.8	
<u>CB-CaCO3</u> (XI)	3.6 ± 1.0	1.6 ± 0.4	0.0011	9.2	
<u>CB-CaCO3</u> * (XII)	3.9 ± 1.5	2.3 ± 0.6	0.0086	1.1	
<u>CB-CaCO₃* (XIII)</u>	0.8 ± 0.1	0.7 ± 0.1	0.0315	0.31	

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- 193 *3.2 Effect of mixing method*
- 194 Ball-milling reduced the CB particle size and size distribution each by a factor of approximately

three (Table 1). The particle size reduction led to an increase in reaction rate (Fig. 2a).



196

195

Fig. 2. CO₂ gasification at 850 °C of a) CB, b) CB with K₂CO₃, and c) CB with CaCO₃. Curve
labels correspond to mixing methods and particle sizes in Table 1.

200 Assuming spherical geometry and completely dense particles, the reduction in particle size should 201 increase the surface area by a factor of 3.4. The measured surface area increased by a factor of 2.8 (from 18 to 50 m^2/g) and the pores sizes increased (from less than 1 nm (Fig. S.1a) up to 25 nm 202 203 (Fig. S.1b) after ball-milling. The maximum gasification rate, however, increased by only a factor 204 of 1.4. One possible explanation for the smaller than expected increase in gasification rate may be 205 the presence of occluded pores within the carbon black that became accessible after ball milling 206 and/or once gasification began. Thus, the surface area of the as received carbon black was 207 underestimated.

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209 When both CB and catalysts were present, ball-milling could result in an increased gasification 210 rate in two ways: by reducing the particle size (increasing specific surface area) and by improving 211 the initial dispersion of the catalyst (increasing interfacial area between carbon and catalyst). To 212 distinguish between these factors, the components were ball-milled separately before hand-mixing 213 (only particle size reduction) and ball-milled together (particle size reduction and catalyst 214 dispersion). Ball-milling reduced the sizes of the CaCO₃ and K_2CO_3 particles to 1.6-1.9 µm 215 (mixtures X and XI, Table 1) and 0.7-0.9 µm (mixtures V and VI, Table 1), respectively. The Mohs 216 hardness values are ~2.5 for a generic carbon black [41] (no specific data was available for Cabot 217 Monarch 120), ~ 3 for CaCO₃ [42], and ~ 8 for zirconia balls [43]. No data was found for K₂CO₃, 218 but the hardness is assumed to be lower than that of the zirconia balls. K₂CO₃ may be harder than 219 $CaCO_3$ as the CB particles were smaller after ball-milling with K_2CO_3 than $CaCO_3$.

220

221 The gasification results for the CB-K₂CO₃ mixtures are shown in Fig. 2b. The highest rates were 222 obtained when K_2CO_3 was ball-milled – without CB being ball-milled (V), the components ball-223 milled separately (VI), or the components ball-milled together (VII) - and the rates for these 224 mixtures (curves V, VI, and VII) were significantly higher than the rates of the other mixtures 225 (curves III and IV). The curves with the three highest rates were within experimental error above 226 40% conversion, though modeling gave different rate constant values, which is discussed further 227 in Section 3.4. The difference in the mixtures corresponding to curves III and IV was the size of 228 the CB particles (7.9 µm and 2.3 µm, respectively). As shown in Fig. 2a, reducing the size of the

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229 CB particles increased the gasification rate but, in the presence of a catalyst, this effect was 230 enhanced. Nonetheless, ball-milling the K₂CO₃ had a larger effect than ball-milling the CB. In the 231 mixture corresponding to curve V, the average CB particle size was 9.2 µm, slightly larger than 232 that in the hand-mixed mixture (7.9 μ m, curve III) and four times larger than that in the mixture 233 corresponding to curve IV (2.3 µm). The results suggest that potassium is more active when ball-234 milled because the smaller crystals are more readily able to disperse. That is, potassium was 235 equally effective as a catalyst whether ball-milled with, or separately from, the CB because of its 236 high mobility.

237

238 Ball-milling CB and/or CaCO₃ led to a reduction in particle size for both the CB and the CaCO₃ 239 (Table 1). As received, the CaCO₃ particles were cubic crystals (Fig. 1c). After ball-milling with 240 or without CB (Fig. 1f), the shapes of the crystals were irregular, although some cubes were still 241 visible in the SEM images. The gasification results were lower and more varied than for the CB-K₂CO₃ mixtures (Fig. 2c). The gasification rate at 50% conversion varied from 0.0006 min⁻¹ for 242 hand-mixed CB-CaCO₃ (VIII) to 0.0086 min⁻¹ for CB-CaCO₃ ball-milled together (XII). The latter 243 244 rate was one third of the rate for hand-mixed CB-K₂CO₃, while the former was less than half of 245 the value for CB as received with no added catalysts. The decrease in particle size (assuming 246 spherical particles for CB throughout and for CaCO₃ after ball-milling – CaCO₃ is cubic before 247 ball-milling) increased the surface areas by a factor of 3.3 for CB and by 1.9 for CaCO₃, which 248 does not account for the 14-fold increase in gasification rate.

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249

250 The interfacial area between the catalyst and substrate was also a factor. The experiments with 251 only CB ball-milled (IX), only CaCO₃ ball-milled (X), or both components ball-milled separately 252 prior to hand-mixing (XI) had the same average rates of reaction ($\sim 0.0015 \text{ min}^{-1}$) but very different 253 reaction rate profiles as a function of conversion. This variation may be due to the heterogeneous 254 nature of hand-mixed samples. In all three cases, the rate of reaction was significantly below that 255 of CB-CaCO₃ ball-milled together (XII) from 10-99% conversion. The propensity of CaCO₃ to 256 sinter above 850 °C has been shown in previous publications [36,44]. Ball-milling the components 257 together more effectively dispersed the CaCO₃ and reduced the extent of sintering. The lower 258 mobility of Ca meant that both the particle size and the interfacial contact area between Ca and 259 CB were critical to the catalytic activity.

260

261 To further compare the behaviors of K₂CO₃ and CaCO₃ prior to gasification, EDX analysis was 262 performed on the hand-mixed mixtures after heating to 850 °C under inert N₂ flow in the TGA 263 (shown in Fig. S.2). The CB-K₂CO₃ mixture had agglomerations containing approximately 6% 264 potassium, 71% carbon, and 23% oxygen. The K₂CO₃ had dispersed on the CB surface during 265 heating to an extent perceptible in the SEM (the reactions will happen at a scale much smaller than 266 that probed by SEM). Ball-milling reduced the crystal size, further creating more potassium active 267 sites that were readily dispersed at gasification temperatures even when not ball-milled directly 268 with the CB. In contrast, there was no evidence in the SEM images that CaCO₃ had dispersed

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269 during heating to 850 °C, with or without ball milling, but remained in the original cubic crystalline

form, consistent with CaCO₃ being a less active catalyst than K₂CO₃.

271

272 In all the CB-CaCO₃ mixtures hand-mixed or ball-milled with 5 mm beads, the particle size of 273 CaCO₃ was at least 1.6 µm (curves VIII to XII, Table 1), which was larger than K₂CO₃ as received 274 (1.5 μ m, Table 1). To test if further reducing the size of the CaCO₃ particles would improve the 275 activity, CB and CaCO₃ were ball-milled using 1 mm quartz glass balls (Mohs hardness of ~ 7 [45] 276 - SEM/EDX analysis did not detect Si or Al from these beads on the mixtures) in addition to the 277 5 mm zirconia balls, and then this CB-CaCO₃ mixture was gasified. After ball-milling with the 278 smaller balls, the CB and the CaCO₃ particles were smaller than the particle sizes in the hand-279 mixed CB-K₂CO₃ mixture (XIII vs. III, Table 1). Reduction of the particle sizes and improved 280 catalyst dispersion increased the gasification rate (Fig. 3). Up to 50% conversion, the gasification 281 rates of CB-CaCO₃ (XIII) and CB-K₂CO₃ (III) were in a similar range, albeit the curve shapes 282 were different (Fig. 3). At higher conversions, the gasification rate with CaCO₃ was much lower 283 than that with K₂CO₃, reflecting the inhibitive sintering of CaCO₃, explored in further depth in 284 Section 3.3.

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285

Fig. 3. CO₂ gasification at 850 °C of CB with either K₂CO₃ or CaCO₃ as added catalysts.

288 *3.3 Gasification inhibition*

289 Both catalysts will inhibit gasification if they sinter and/or block access of CO₂ to the CB. To 290 further illustrate this inhibition, tests were performed with different placements of CB and K₂CO₃ 291 (Fig. 4a) or CaCO₃ (Fig. 4b, note the different y-axis range than in Fig. 4a) within the crucible. 292 The total weight was always within 0.1 mg of the target weight, the catalysts were used as received 293 (particles sizes of 1.5 µm for K₂CO₃ and 7.1 µm for CaCO₃, Table 1), and the CB was ball-milled 294 (particle size of 3.1 µm, Table 1). The gasification rates were generally higher when the catalyst 295 was placed below the CB. For the samples with CB and K₂CO₃, the curves had similar shapes regardless of the location of the catalyst with the gasification rates decreasing in the order of K₂CO₃ 296 297 on bottom > hand-mixed > K_2CO_3 on top. For the samples with CB and CaCO₃, the curves had

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- 298 different shapes. The gasification rate decreased exponentially for the hand-mixed sample and was
- 299 nearly an order of magnitude higher initially than those of the other samples for which the curve
- 300 shapes were concave-down and had rates decreasing in the order $CaCO_3$ on bottom > CB > CaCO_3
- 301 on top. That is, placing CaCO₃ on top of the CB severely inhibited the reaction.



302

Fig. 4. CO₂ gasification of ball-milled CB at 850 °C with different placement of a) K₂CO₃, and b)
 CaCO₃ relative to CB.

305

The Tammann softening temperature (i.e. two-thirds of the melting point) of CaCO₃ is 842 °C. CaCO₃ heated to 850 °C under CO₂ then cooled to room temperature formed a fused solid in the crucible. If heated under N₂, which allowed CaCO₃ to decompose to CaO (the Tammann softening temperature of CaO is 1624 °C), a loose powder remained in the crucible. The more dispersed the CaCO₃ was initially (e.g., by ball-milling the mixture together, CB-CaCO₃ (XII) in Fig. 2c), the higher the conversion that could be reached before the CaCO₃ formed a continuous phase through which CO₂ had to diffuse before reacting with the CB. Indeed, sintering is reported as the primary

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- 313 mode by which calcium gasification catalysts deactivate [44]. The formation of the sintered layer
- 314 can be avoided by heating the mixtures in N₂ and gasifying at temperatures where CaO rather than
- 315 CaCO₃ is stable. The gasification of ball-milled CB by itself (CB (II)) or hand-mixed with CaCO₃
- 316 (CB-CaCO₃ (IX)) at 1000 °C demonstrates this idea. At this temperature, calcium remained as
- 317 CaO even in a ~98% CO₂ atmosphere and thus, the Ca-catalyzed gasification of CB was not
- 318 inhibited by sintering (Fig. 5). Thus, conditions (temperature, concentration) at which CaCO₃ will
- 319 sinter should be avoided where possible.



320

Fig. 5. Conversion versus time curves for CO₂ gasification at 1000 °C of ball-milled CB and handmixed with CaCO₃.

323

- 324
- 325 3.4 Kinetic modeling

For quantification, the gasification results were fit to two models – RPM and eRPM. The data were not well fit by the RPM, but the rate constants, k, from this fit were used as the k-values for the

328 eRPM modeling to estimate the parameters ψ , c, and p as shown in Table 2. The fits for the

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329 gasification rates of all the CB-K₂CO₃ mixtures had R^2 values above 0.96. The values of k_i were as expected, with ball-milled mixtures having higher values than hand-mixed mixtures, and K₂CO₃ 330 331 showing values one to two orders of magnitude higher than CaCO₃. Though curves V, VI, and VII 332 (Fig. 2b) were indistinguishable above 40% conversion, the k_i values were significantly different. 333 The value was highest for ball-milled K₂CO₃ which was subsequently hand-mixed with CB as 334 received (V), suggesting that ball-milling the CB had no discernible effect on gasification rates 335 when the K₂CO₃ particle size had been reduced by ball-milling. The values of ψ for CB-K₂CO₃ 336 mixtures reflected that the higher dispersions achieved through ball-milling of K₂CO₃ increased 337 pore development. The p values were much smaller for samples in which K_2CO_3 was ball-milled, 338 reflecting lower conversions for the maximum gasification rates (Fig. 1b). Ball-milling of K₂CO₃ 339 increased the initial rate of porosity generation, and hence the initial gasification rate. No trend 340 was observed in the c values for CB-K₂CO₃, similar to a previous study on coal gasification [32]. 341

In the case of the CB-CaCO₃ samples, mixtures VIII and XI had similar gasification profiles as the CB samples and, therefore, the eRPM did not fit the data well. The eRPM was the best fit when CB and CaCO₃ were ball-milled together, further demonstrating that calcium was most effective as a gasification catalyst when reduced in particle size and well-dispersed. The structural parameter, ψ , for the gasification of the CB-CaCO₃ samples in which only CB was ball-milled (curve IX) or in which only CaCO₃ was ball-milled (curve X) was zero. That is, there was no porosity development, consistent with calcium sintering rather than moving through the CB

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349 particles. Ball-milling the CB and CaCO₃ together (curve XII) better dispersed the catalyst and

allowed porosity to develop ($\psi = 11.3$) before the catalyst sintered. Overall, the eRPM modeling

351 results reflect the importance of the mixing method: ball-milling better dispersed the catalysts

352 leading to increased porosity development and thus, higher reaction rates for both potassium and

353 calcium. Better dispersion also impeded the rate of CaCO₃ sintering.

354

Table 2. Rate constants (k_j), structural factors (ψ), and R^2 values for the catalytic CB samples calculated by the extended random pore model (eRPM) with a 95% confidence interval. Underlined components were ball-milled; mixtures with an asterisk (*) were ball-milled together.

Sample	k	Ψ	С	р	R^2
CB-K ₂ CO ₃ (III)	$3.2 \cdot 10^{-2} \pm 4.5 \cdot 10^{-4}$	1.98 ± 0.11	0.45 ± 0.04	13.92 ± 1.64	0.954
<u>CB</u> -K ₂ CO ₃ (IV)	$1.1 \cdot 10^{-1} \pm 1.3 \cdot 10^{-3}$	0.92 ± 0.03	-0.63 ± 0.03	24.89 ± 2.00	0.971
$CB-\underline{K_2CO_3}(V)$	$3.2 \cdot 10^{-1} \pm 4.8 \cdot 10^{-3}$	18.83 ± 1.29	$\textbf{-0.48} \pm 0.01$	$\textbf{-0.21} \pm 0.01$	0.980
\underline{CB} - $\underline{K_2CO_3}$ (VI)	$2.5 \cdot 10^{-1} \pm 5.1 \cdot 10^{-3}$	66.94 ± 0.00	-0.63 ± 0.00	$\textbf{-0.13} \pm 0.00$	0.990
$\underline{\text{CB-K}_2\text{CO}_3^*}$ (VII)	$2.2 \cdot 10^{-1} \pm 4.4 \cdot 10^{-3}$	58.19 ± 4.71	$\textbf{-0.56} \pm 0.02$	$\textbf{-0.15} \pm 0.01$	0.990
<u>CB</u> -CaCO ₃ (IX)	$1.6 \cdot 10^{-3} \pm 3.8 \cdot 10^{-5}$	0.00 ± 0.00	7.23 ± 0.09	8.19 ± 0.10	0.973
$CB-\underline{CaCO_3}(X)$	$2.6{\cdot}10^{\text{-3}} \pm 3.9{\cdot}10^{\text{-5}}$	0.00 ± 0.00	0.13 ± 0.00	$\textbf{-1.06} \pm 0.00$	0.818
<u>CB-CaCO₃*</u> (XII)	$3.7 \cdot 10^{-3} \pm 1.6 \cdot 10^{-4}$	11.31 ± 0.21	0.39 ± 0.01	$\textbf{-5.92} \pm 0.00$	0.992

³⁵⁸

The maximum rates observed for ball-milled K₂CO₃ (> 0.3 min⁻¹, Fig. 2b) are an order of magnitude higher than those observed in the literature for feeds such as coal [47] and biomass [16,48]. Rates greater than 0.1 min⁻¹ have been observed in our previous studies with CB [35,36], suggesting that the extremely high rates are due to the properties of the CB, including the absence of ash, the highly amorphous nature, and the low porosity (18 m²/g by CO₂ physisorption). These high rates, however, are likely mass transfer limited. The high ψ -values for mixtures VI and VII indicate the creation of porosity, which would be expected to lead to even higher reaction rates in

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366 the absence of mass transfer limitations. For Ca-catalyzed gasification at 850 °C, the highest rates 367 are an order of magnitude lower than the slowest rates for K-catalyzed gasification. The sintering 368 of CaCO₃ at high conversions will introduce mass transfer limitations. The presence of mixed 369 kinetic-transport control for mixtures V-VII does not affect the overall conclusions of the paper; 370 namely, Ca is most effective as a gasification catalyst when reduced in particle size and well-371 dispersed with the gasification feed, while K is most effective when reduced in particle size, as the 372 dispersion within the feed is less of a factor due to the high mobility of K at typical gasification 373 temperatures.

374

375 *3.5 Applications for future studies*

376 Particle sizes of the feed and catalytic species are rarely provided in literature results, but the trends 377 of particle sizes or catalyst surface area versus gasification rates have been discussed. Studies vary 378 from finding slight increases in gasification rate with a reduction in particle size [49] to finding 379 dramatic increases [50]. There is also a high variability in what is considered a reduced particle 380 size; for example, one study [8] estimated 1 mm as the particle size below which diffusion 381 limitations are insignificant, suggesting that further particle size reduction was ineffective for 382 increasing the reaction rate. Our results, however, indicate that the reaction rate increased in the 383 absence of catalysts when decreasing the CB particles from 10.6 to 3.1 µm (Fig. 2a), demonstrating 384 that diffusion limitations were still present in carbon particles much smaller than 1 mm in diameter. 385 In the aforementioned study [8], the feed was highly porous (reported surface area of 620 m^2/g),

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more than 30 times larger than the specific surface area of the CB in our study. For highly porous feeds, reducing the particle size would have a negligible effect on the specific surface area. Increasing the specific surface area would also have a negligible effect for systems in which external mass transfer was the limiting factor. The properties of the feed, including particle size and specific surface area, should be given in all gasification papers to allow for comparison between varied feeds.

392

393 The particle size of the catalyst has a much larger effect on the overall reaction rate than the particle 394 size of the CB, and this effect increases with increasing temperature. At 700 °C, a six-fold 395 reduction in catalyst size led to an increase in the reaction rate by a factor of 2.3 [51], while at 396 900 °C, a two-fold reduction in particle size led to an increase in the reaction rate by a factor of 397 4.5 [52]. Increased calcium loading up to approximately 4 wt% led to an increase in reaction rate, 398 but higher loadings did not lead to a further increase because of the increase in sintering [53]. This 399 sintering of CaCO₃ has also been observed over time, with the rate of reaction decreasing by a factor of 25 after an hour of gasification at 700 °C despite not reaching complete conversion [51]. 400 401 The results with calcium in the current study observed sintering taking place over time (Fig. 4b). 402 No studies could be found in which the particle size of a potassium catalyst was given. For 403 meaningful comparisons between gasification studies, the particle sizes of all catalysts used should 404 be provided.

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406 The rate of gasification has also been found to increase with increased calcium catalyst dispersion 407 [44,54–56]. CaO has been observed to be more effective as a catalyst when added using ion 408 exchange than wet impregnation due to the low solubility of CaO in water [52,57]. Our study 409 established that increased dispersion and reduced particle size both have a significant effect on the 410 gasification rate when CaCO₃ is used as the catalyst, while only initial particle size has a significant 411 effect when K₂CO₃ is used as the catalyst. The current study also found that CaCO₃ can inhibit the 412 gasification rate if not sufficiently dispersed, which has not been discussed in the literature. When 413 reporting sample preparation techniques in gasification papers, a phrase such as "physical mixing" 414 should not be used, since it encompasses a variety of techniques from briefly stirring with a spatula to high-energy planetary ball-milling. Details of the mixing method used should be provided, and 415 416 the extent of pre-gasification catalyst dispersion should be at least qualitatively assessed in future 417 gasification publications.

418

419 4. Conclusions

The catalyst introduction technique has a significant effect on the rates observed in gasification as shown in this study with CB and K₂CO₃ or CaCO₃. The less active and/or mobile the catalyst, the more impact parameters such as feed particle size, catalyst particle size, and dispersion have on the gasification rates. In addition, the phase behavior of the catalyst must be considered. For example, when CaCO₃ was insufficiently dispersed, it sintered and surrounded the carbon, which reduced access of the gasification agent, CO₂, to the CB. Conversely, the gasification rates using a high-mobility catalyst such as K₂CO₃ were only dependent on catalyst particle size, with the

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427 calculated rates and modeled rate constants being independent of carbon particle size or catalyst 428 dispersion. The eRPM modeling results identified, through the changes in the structural parameter 429 ψ , that the catalyst dispersion increased the creation of porosity during gasification. With Ca, porosity formation was only observed when the carbon and catalyst were ball-milled together, 430 431 while with K, ball-milling greatly increased the porosity generation. These results highlight the 432 significantly different rates that can be obtained depending on the properties of the feed mixture. 433 Details of particle sizes and catalyst dispersion must always be reported to allow for appropriate 434 comparison within and between studies.

435

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